

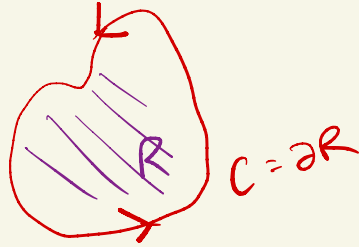
9-3:

Recall: Big theorem

$$\iint_R \text{"derivative f"} \cdot dA = \int_{\partial R} \text{"f"} \cdot d\vec{r}$$

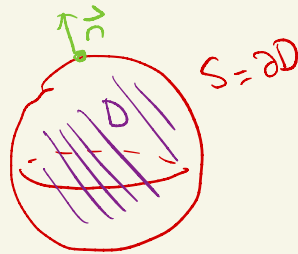
\uparrow
surface

\uparrow
boundary of surface



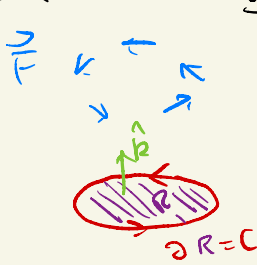
and

$$\iiint_D \text{"derivative f"} \cdot dV = \iint_S \text{"f"} \cdot \vec{n} \, d\sigma$$

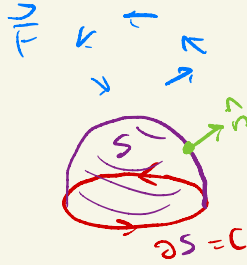


Extending Green's theorems to 3D

- Stokes' theorem extends Green's curl-circulation theorem to any surface R with boundary $\partial R = C$:



Green's (integral)



Stokes' Theorem

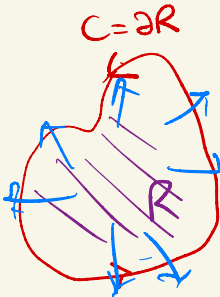
$$\iint_R (\nabla \times \vec{F}) \cdot \vec{n} \, dA = \oint_{\partial R} \vec{F} \cdot d\vec{r}$$

$$\iint_S (\nabla \times \vec{F}) \cdot \vec{n} \, d\sigma = \oint_{\partial S} \vec{F} \cdot d\vec{r}$$

Green's Thm (normal)

$$\iint_R (\nabla \cdot \vec{F}) \, dx \, dy = \oint_{\partial R} \vec{F} \cdot \vec{n} \, ds$$

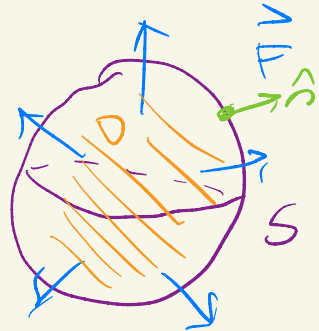
Total divergence inside = outward flux boundary



Divergence Theorem

$$\iiint_D \nabla \cdot \vec{F} \, dV = \iint_S \vec{F} \cdot \vec{n} \, d\sigma$$

Total divergence inside = outward flux boundary



16.7: Stokes and Divergence Theorems

Reminder: pay attention to "type" of object.

• $f(x, y, z) \leftarrow$ scalar function

• $\vec{F}(x, y, z) = \langle M, N, P \rangle \leftarrow$ vector field

Notation: $\nabla = \left\langle \frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \right\rangle$

• Gradient:

$$\nabla f = \left\langle \frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \right\rangle f = \left\langle \frac{\partial f}{\partial x}, \frac{\partial f}{\partial y}, \frac{\partial f}{\partial z} \right\rangle \leftarrow \text{vector field}$$

• Divergence:

$$\text{div } \vec{F} = \nabla \cdot \vec{F} = \frac{\partial M}{\partial x} + \frac{\partial N}{\partial y} + \frac{\partial P}{\partial z} \leftarrow \text{scalar function}$$

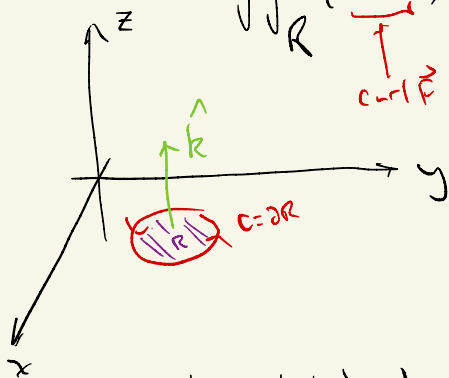
• Curl:

$$\text{curl } \vec{F} = \nabla \times \vec{F} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ M & N & P \end{vmatrix} \leftarrow \text{vector field}$$
$$= \left(\frac{\partial P}{\partial y} - \frac{\partial N}{\partial x} \right) \hat{i} - \left(\frac{\partial P}{\partial x} - \frac{\partial M}{\partial z} \right) \hat{j} + \left(\frac{\partial N}{\partial x} - \frac{\partial M}{\partial y} \right) \hat{k}$$

Recall: Green's thm (curl-circulation form)

$$\iint_R (\nabla \times \vec{F}) \cdot \hat{k} dA = \oint_C \vec{F} \cdot d\vec{r}$$

\uparrow $\text{curl } \vec{F}$



Good example: whirlpool

$$\vec{F} = -y\hat{i} + x\hat{j}$$

$$\text{curl } \vec{F} = 2\hat{k}$$

$$\oint_{\text{unit circle ccw}} \vec{F} \cdot d\vec{r} = 2\pi$$

\uparrow $\text{curl } \vec{F}$ \leftarrow max unit circle

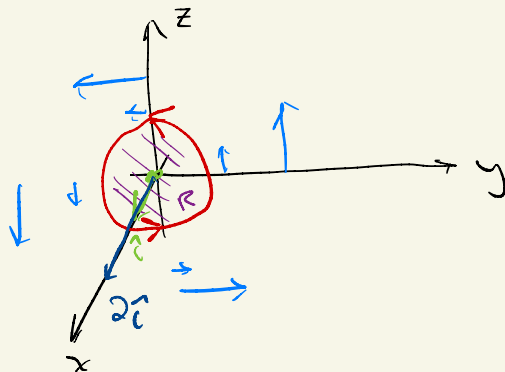
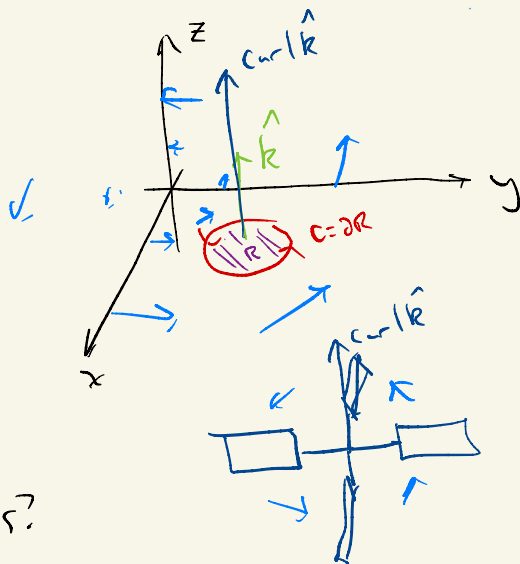
What about other whirlpools?

$$\vec{F} = -z\hat{j} + y\hat{k}$$

$$\text{curl } \vec{F} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ 0 & -z & y \end{vmatrix}$$

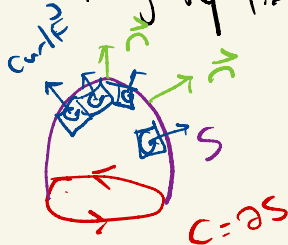
$$= (1+1)\hat{i}$$

$$= 2\hat{i}$$

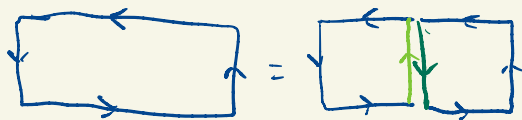


Idea: $\text{curl } \vec{F}$ detects plane rotation of \vec{F} and places it in normal vector to plane of rotation

Now: take any surface S with boundary $\partial S = C$.
 can break into tiny pieces which look
 roughly linear (like little planes!)



Like Green's thm:



orientation
 of S is determined
 by right-hand
 rule on oriented curve C

"3D Green's Thm"

\vec{n} determines
 orientation
 "inside" vs. "outside"

Stokes' Theorem

Let S be a piecewise smooth oriented surface
 with a piecewise smooth boundary $C = \partial S$

If \vec{F} is a vector field with continuous 1st derivatives,
 then

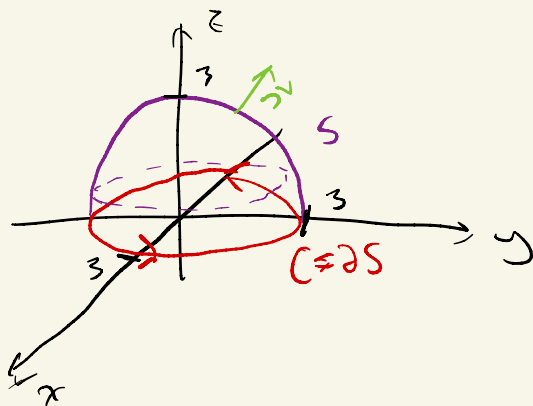
$$\oint_{\substack{\partial S \\ C = \partial S}} \vec{F} \cdot d\vec{r} = \iint_S (\underbrace{\nabla \times \vec{F}}_{\text{curl } \vec{F}}) \cdot \vec{n} \, d\sigma$$

Ex:

compute $\iint_S (\nabla \times \vec{F}) \cdot \vec{n} d\sigma$ where

$$S = \text{half sphere} \\ x^2 + y^2 + z^2 = 9 \\ z \geq 0$$

$$\vec{F} = y\hat{i} - x\hat{j}$$



Soln:

Option 1: Dot the surface integral!

Option 2: Stokes:

$$\iint_S (\nabla \times \vec{F}) \cdot \vec{n} d\sigma = \oint_C \vec{F} \cdot d\vec{r}$$

↑
calculate this!

$$\vec{r}(t) = 3\cos t \hat{i} + 3\sin t \hat{j} \\ 0 \leq t \leq 2\pi$$

$$\vec{r}'(t) = -3\sin t \hat{i} + 3\cos t \hat{j}$$

$$\vec{F} = y\hat{i} - x\hat{j}$$

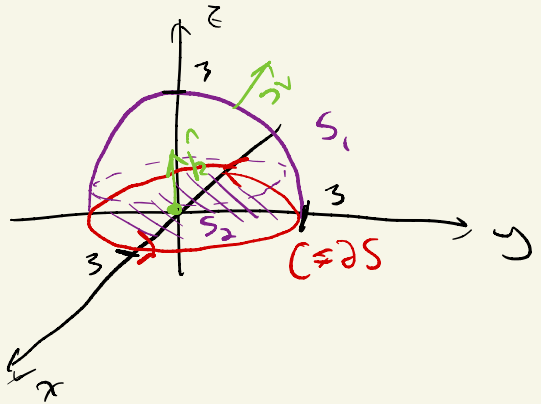
$$\begin{aligned} \vec{F} \cdot \vec{r}'(t) &= (3\sin t \hat{i} - 3\cos t \hat{j}) \cdot (-3\sin t \hat{i} + 3\cos t \hat{j}) \\ &= -9\sin^2 t - 9\cos^2 t \\ &= -9 \end{aligned}$$

$$\begin{aligned} \Rightarrow \iint_S (\nabla \times \vec{F}) \cdot \vec{n} d\sigma &= \oint_C \vec{F} \cdot d\vec{r} = \int_0^{2\pi} -9 dt \\ &= -18\pi \end{aligned}$$

Surprise Option 3:

S_1 = half sphere

S_2 = disc of radius 3
in xy



$$\iint_{S_1} (\nabla \times \vec{F}) \cdot \vec{n} \, d\sigma = \oint_C \vec{F} \cdot d\vec{r}$$

Stokes

$$\hookrightarrow \iint_{S_2} (\nabla \times \vec{F}) \cdot \vec{n} \, d\sigma$$

$$= \iint_{S_2} (\nabla \times \vec{F}) \cdot \hat{k} \, dA$$

← since S_2 in xy plane

$$\nabla \times \vec{F} = \left(\frac{\partial}{\partial x}(-x) - \frac{\partial}{\partial y}(y) \right) \hat{k}$$

$$= -2\hat{k}$$

← For this problem, $\nabla \times \vec{F}$ only has a \hat{k} component. However,

if $\nabla \times \vec{F}$ had more than a \hat{k} component,

since we are about

$(\nabla \times \vec{F}) \cdot \hat{k}$ only the \hat{k} component because everything else will die.

$$\Rightarrow \iint_{S_2} (\nabla \times \vec{F}) \cdot \hat{k} \, dA = \iint_{\bigcirc_{\frac{1}{3}}^{\frac{3}{3}}} (-2\hat{k}) \cdot \hat{k} \, dA$$

$$= -2 \iint_{\bigcirc_{\frac{1}{3}}^{\frac{3}{3}}} dA$$

$$= -2 \left(\frac{3^2}{3} \pi \right) = \boxed{-18\pi}$$

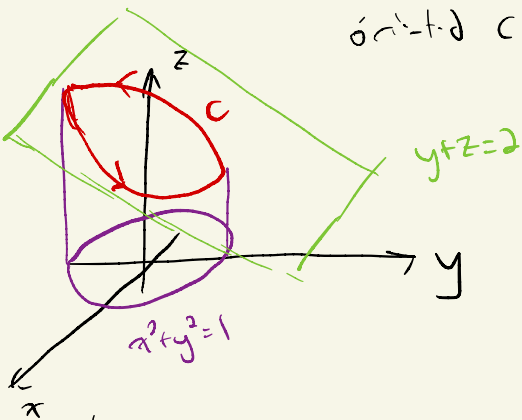
Ex:

Evaluate $\oint_C \vec{F} \cdot d\vec{r}$, $\vec{F} = -y^2 \hat{i} + x \hat{j} + z^2 \hat{k}$

$C =$ intersection of plane $y+z=2$

cylinder $x^2+y^2=1$

oriented CCW from above



Soln:

Option 1: Do the line integral (parametrizing won't be tedious.)
Not too bad though

Option 2: Stokes theorem:

$$\oint_C \vec{F} \cdot d\vec{r} = \iint_S (\nabla \times \vec{F}) \cdot \vec{n} d\sigma$$

two choices



Depending on the vector field,
more complicated surfaces can have
easier integrals

$$\begin{aligned} \nabla \times \vec{F} &= \left(\frac{\partial}{\partial y}(z^2) - \frac{\partial}{\partial z}(x) \right) \hat{i} \\ &\quad - \left(\frac{\partial}{\partial x}(z^2) - \frac{\partial}{\partial z}(-y^2) \right) \hat{j} \\ &\quad + \left(\frac{\partial}{\partial x}(x) - \frac{\partial}{\partial y}(y^2) \right) \hat{k} \\ &= (1+2y) \hat{k} \end{aligned}$$

S₁



well, level surface

$$g(x, y, z) = y + z - 2 = 0$$

$$\Rightarrow \vec{n} = \frac{\nabla g}{|\nabla g|}$$

$$= \frac{1}{\sqrt{2}} \hat{j} + \frac{1}{\sqrt{2}} \hat{k}$$

Explicit surface:

$$\iint_{S_1} (\nabla \times \vec{F}) \cdot \vec{n} \, d\sigma = \iint_{\text{unit disc in } xy} (1+2y) \hat{k} \cdot \left(\frac{1}{\sqrt{2}} \hat{j} + \frac{1}{\sqrt{2}} \hat{k} \right) \sqrt{f_x^2 + f_y^2} \, dA$$

$f(x, y) = z = -y + 2$

$$= \iint_{\text{unit disc}} \frac{1}{\sqrt{2}} (1+2y) \cdot \sqrt{0^2 + 1^2} \, dA$$

$$= \int_0^{2\pi} \int_0^1 (1+2r \sin \theta) r \, dr \, d\theta$$

$$= \pi$$

level surface for cylinder:
 $x^2 + y^2 = 1 \Rightarrow (x+y)^2 + z^2 = 1$
 $\vec{n} = \frac{\nabla g}{|\nabla g|}$

$$\vec{n} = \hat{k}$$

$\vec{n} \perp \hat{k}$
 $\Rightarrow \vec{n} \cdot \hat{k} = 0$ on sides
 \downarrow

S₂



$$\iint_{S_2} (\nabla \times \vec{F}) \cdot \vec{n} \, d\sigma = \iint_{\text{bottom}} (1+2y) \hat{k} \cdot \vec{n} \, d\sigma + \iint_{\text{sides}} (1+2y) \hat{k} \cdot \vec{n} \, d\sigma$$

$$= \iint_{\text{unit disc}} (1+2y) \hat{k} \cdot \hat{k} \, dA + 0$$

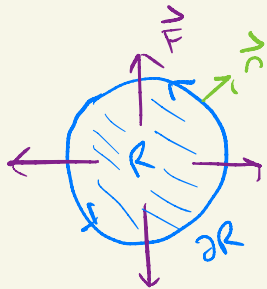
$$= \iint_{\text{unit disc}} 1+2y \, dA$$

$$= \pi$$

16.8 Divergence Theorem

Recall: Green's theorem (flux-divergence form)

$$\oint_{\partial R} \vec{F} \cdot \vec{n} \, ds = \iint_R \underbrace{\nabla \cdot \vec{F}}_{\text{div } \vec{F}} \, dA$$



"flux on boundary detects amount of source/sink inside"

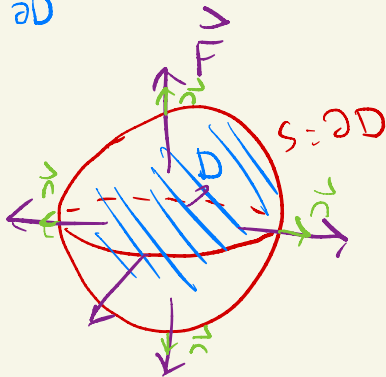
Divergence theorem says this idea should work in 3D as well!

Divergence Theorem:

Let \vec{F} a vector field with continuous first derivatives on S a piecewise smooth closed surface enclosing D .

The outward flux of \vec{F} across S is

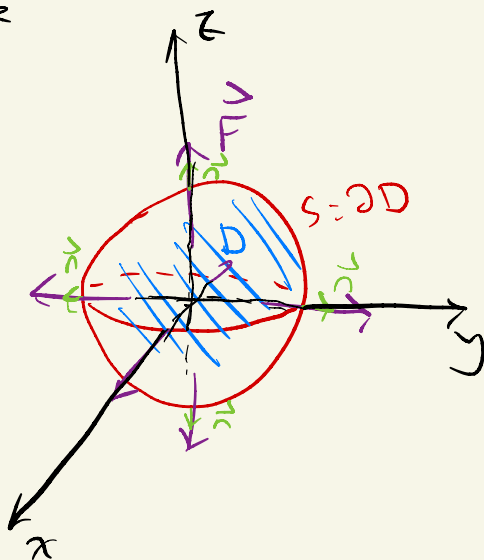
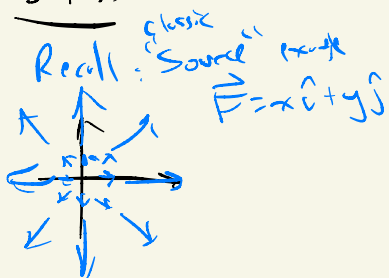
$$\oint_{\substack{S \\ \partial D}} \vec{F} \cdot \vec{n} \, d\sigma = \iiint_D \underbrace{\nabla \cdot \vec{F}}_{\text{div } \vec{F}} \, dV$$



Ex:

Find the flux of $\vec{F} = x\hat{i} + y\hat{j} + z\hat{k}$
through sphere $x^2 + y^2 + z^2 = a^2$

Soln:



Option 1: Do the surface integral

Implicit: $g(x, y, z) = x^2 + y^2 + z^2 - a^2 = 0$

$$\Rightarrow \vec{n} = \frac{\nabla g}{|\nabla g|} = \frac{2(x\hat{i} + y\hat{j} + z\hat{k})}{\sqrt{4(x^2 + y^2 + z^2)}} = \frac{x\hat{i} + y\hat{j} + z\hat{k}}{a}$$

↑
same direction
as \vec{F}

$$\Rightarrow \vec{F} \cdot \vec{n} = |\vec{F}| \cdot |\vec{n}| = |\vec{F}|$$

↑
unit vector
in F direction

$$= \sqrt{x^2 + y^2 + z^2} = a$$

$$\oiint_S \vec{F} \cdot \vec{n} \, d\sigma = \oiint_S a \, d\sigma$$

$$= a \oiint_S d\sigma$$

$$= a \cdot \text{surface area}$$

$$= 4\pi a^2 \cdot a$$

$$= 4\pi a^3$$

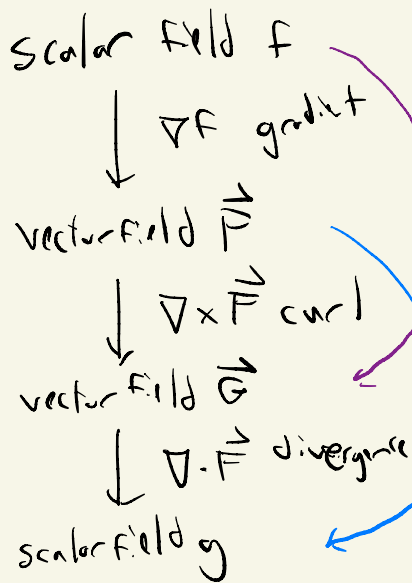
Option 2: Divergence Thm

$$\nabla \cdot \vec{F} = \frac{\partial}{\partial x}(x) + \frac{\partial}{\partial y}(y) + \frac{\partial}{\partial z}(z) = 3$$

$$\begin{aligned}\oint_S \vec{F} \cdot \vec{n} \, d\sigma &= \iiint_D 3 \, dV = 3 \iiint_D dV \\ &= 3 \operatorname{Vol}(\text{sphere}) \\ &= 3 \left(\frac{4}{3} \pi a^3 \right) \\ &= 4 \pi a^3\end{aligned}$$



In \mathbb{R}^3 :



$$\nabla \times (\nabla f) = 0$$

"curl of gradient is 0"
(conservative!)

$$\nabla \cdot (\nabla \times \vec{F}) = 0$$

"divergence of the curl is 0"

Def:

Irrrotational:
(curlless)

$$\nabla \times \vec{F} = 0$$

(aka \vec{F} conservative)

← component test

Incompressible:
(divergenceless)

$$\nabla \cdot \vec{F} = 0$$

consequence:

- Gradients are irrotational
- curls are incompressible